

ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024 CFD STUDIES ON A DOWNDRAFT BIOMASS GASIFIER

#### Mugdha Bhamare, K. B. Sutar

Department of Mechanical Engineering, Bharati Vidyapeeth (Deemed to be University), College of Engineering, Pune-411043, Maharashtra, India. 1 pmugdha300@gmail.com, 1 kbsutar@bvucoep.edu.in

#### ABSTRACT

Computational Fluid Dynamics (CFD) studies on downdraft gasifiers provide valuable insights into the complex physical and chemical processes involved in biomass gasification. Downdraft gasifiers, commonly used for small- to medium-scale biomass-to-energy conversion, offer advantages such as reduced tar formation and the ability to handle various feedstocks. CFD simulations enable detailed analysis of the gasification process, including the flow of gases, temperature distribution, and chemical reactions, all of which are critical for optimizing performance and efficiency. The present work reports CFD studies of a downdraft biomass gasifier. It highlights key findings related to gas flow dynamics, temperature profiles and pressure distribution. These simulations help identify critical factors affecting gasifier performance, such as air-to-fuel ratios, feedstock properties, and reactor geometry. A two dimensional steady state model of a gasifier was prepared. Grid independency study was conducted prior to finalizing the optimum grid size. The model accurately predicts velocity, pressure and temperature distribution in different zones of the gasifier. The role of CFD in advancing gasification technology is crucial to promoting sustainable energy production and optimizing waste-to-energy systems.

Keywords: Computational Fluid Dynamics (CFD), Downdraft Gasifier, Biomass Gasification, Syngas

#### I. Introduction

This section provides an overview of gasification technology, highlighting its historical evolution, key principles, and the importance of syngas production in the context of renewable energy sources and sustainable development. Biomass, a term got from "natural mass," alludes to natural materials, prevalently plant and creature build-ups that can be used as a sustainable wellspring of energy. This diverse category encompasses a wide range of biological materials, including wood, crop residues, agricultural by-products, and organic waste from households and industries. Unlike fossil fuels, biomass is considered a renewable energy source because the organic matter it comprises can be replenished over relatively short periods through natural processes. A downdraft gasifier is a widely used technology for converting biomass and other carbon-rich feedstocks into synthesis gas (syngas), which can be used for energy production, heat generation, and chemical synthesis. Unlike other types of gasifiers, such as updraft or fluidized-bed systems, the downdraft configuration forces gases to flow downward through the reactor, passing through combustion and reduction zones. This design significantly reduces tar formation-a common challenge in biomass gasification and enables the production of cleaner syngas, making downdraft gasifiers a favourable option for decentralized energy production. Quite possibly of the main contamination in gasification process is tar. It is a dim, thick, combustible fluid refined from feedstock, comprising of a combination of hydrocarbons, tars, and other compounds. To diminish gas tar fixation, a few specialists have been working in the execution of an essential technique for tar transformation [1]. The optimization of downdraft gasifiers requires a thorough understanding of the complex interactions between fluid flow, heat transfer, and chemical reactions within the reactor. This is where Computational Fluid Dynamics (CFD) plays a critical role. CFD simulations offer a powerful tool to model and analyse the various processes occurring in a gasifier, providing insights that are often difficult to obtain through experimental methods alone. By simulating the gasification process, researchers can predict key parameters like temperature distribution, flow patterns, reaction rates, and syngas composition, all of which influence the efficiency and performance of the gasifier. The serious issue worried about biomass is its massiveness, because



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

of which badly designed for transportation, handling, and putting away. This issue inspired the specialists for advancement of change cycles to change over strong biomass into fluid and vaporous structures which can be effectively movable, took care of and put away [2]. The introduction of CFD in downdraft gasifier studies has enabled more precise control over design and operational parameters, leading to improvements in syngas quality, energy efficiency, and overall system reliability. This paper explores the advancements in CFD modelling of downdraft gasifiers, summarizing recent findings and highlighting the potential for further research to enhance gasifier performance and foster the adoption of gasification technology in sustainable energy systems. The essential focal point of the ongoing paper is to analyse and evaluate the application of Computational Fluid Dynamics (CFD) in studying downdraft gasifiers, with a particular emphasis on improving their design, operational efficiency, and syngas production quality. By leveraging CFD simulations, the paper aims to provide a deeper understanding of the intricate interactions between fluid dynamics, heat transfer, and chemical reactions within the gasification process. Ultimately, the paper seeks to highlight the critical role of CFD in optimizing downdraft gasifiers for sustainable energy production and efficient waste-to-energy conversion. Maya et al. [1] utilized a mixed-complexity modelling technique to develop a 3D CFD model aimed at predicting syngas production from Miscanthus briquettes in a two-stage downdraft gasifier, with different gasification fluids. The research was conducted under steady-state conditions using the Ansys Fluent platform and incorporated the non-premixed combustion model. Additionally, a probability density function was applied to describe the chemical kinetics and predict the syngas composition, focusing on the main reactions occurring during gasification. This method was designed to lower computational costs while maintaining prediction accuracy. Gomez et al. [2] described an experimental study that characterized blends of crop residue biomass to assess their energy potential in a commercial-scale downdraft gasifier. The study utilized corncobs, rice husks, sesame stalks, and cotton gin refuse to investigate the impact of mixture ratios on parameters such as equivalence ratio, gasification temperature, syngas lower heating value (LHV), and cold gas efficiency (CGE). A total of thirty-two blends were tested using an Ankur WBG-30 downdraft gasifier, which operates at a feed rate of 30 kg/h and is equipped with a syngas purification system, temperature sensors, and a gas chromatograph. For each blend, the syngas composition- CO, H<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>, and CO<sub>2</sub>-was analysed. The findings indicated that increasing the proportion of rice husks in the blend had a negative effect on gasification temperature, syngas composition, LHV, and CGE. Pandey et al. [3] developed a CFD model for a 2D axisymmetric representation of an Imbert downdraft gasifier, which was validated against experimental data. The model accurately predicts the concentrations of CO, hydrogen, and CO<sub>2</sub> in the producer gas. The study explored the effects of varying equivalence ratios (ER) from 0.25 to 0.60 on gas composition and gasifier temperature. The results show that as the equivalence ratio increases, the amounts of CO, hydrogen, and methane in the producer gas decrease, while nitrogen and CO<sub>2</sub> concentrations rise significantly. Additionally, the temperature within the gasifier increases with higher equivalence ratios. Sharma et al. [4] noted that India, the second most populous country, had an estimated 68.84% of its population residing in rural areas according to the 2011 census. Additionally, approximately 1.79 million km<sup>2</sup> of land in India is dedicated to agriculture, resulting in a significant amount of biomass from agricultural residues during harvest and post-processing. The Ministry of New and Renewable Energy reported that around 500 metric tons of agricultural field residues are generated annually, with 25% classified as surplus, often either burned in fields or wasted in other forms. Instead of large gasification power plants, small-scale pilot power plants should be developed to harness this biomass energy for local applications in rural areas. Jahromi et al. [5] developed a CFD model to simulate the biomass gasification process in a downdraft fixed-bed gasifier, using sugarcane bagasse as the feedstock for both experimental and simulation studies. Various operational parameters were examined, such as the velocity and preheating temperature of the inlet air/steam mixture, the steam-to-air ratio (S/A), and the moisture content (MC) of the biomass, with the goal of optimizing syngas yield (CO<sub>2</sub>, H<sub>2</sub>, CH<sub>4</sub>, and CO) and conversion efficiency. The results indicated that the highest syngas yield and conversion efficiency were achieved with an S/A ratio of

UGC CARE Group-1



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

0.67 and an inlet velocity of 20 m/s. Additionally, increasing the air/steam preheating temperature and reducing the moisture content of bagasse positively influenced the gasification performance. Lewin et al. [6] developed a model for a downdraft gasifier using air to co-gasify municipal solid waste (MSW) and sugarcane bagasse, employing a kinetic, one-dimensional, and steady-state approach. A central composite design was used to evaluate the effects of the co-gasification ratio (CGR), which represents the mass fraction of MSW in the feedstock, along with biomass moisture content and equivalence ratio. As a result, polynomial models were generated to predict syngas composition, lower heating value (LHV), energy efficiency, and the combined molar fractions of CO and H2 on a wet basis. These models demonstrated robustness, with the coefficient of determination (R<sup>2</sup>) values ranging from 0.96 to 0.99.

#### 1. Biomass Gasifier System

A gasifier is system that converts carbonaceous materials, such as biomass, coal, or municipal solid waste, into a combustible gas mixture known as synthesis gas (syngas). This conversion process, called gasification, occurs through the partial combustion of the feedstock in a controlled environment with a limited amount of oxygen or air. The primary purpose of a gasifier is to produce syngas, which can be utilized for electricity generation, heat production, or as a feedstock for chemical synthesis.

The gasifying medium is the substance used to facilitate the conversion of solid or liquid fuel into syngas during gasification. The type of gasifying medium used significantly influences the composition and quality of the produced syngas. Common gasifying media include air, oxygen, steam, and carbon dioxide (CO<sub>2</sub>), each offering distinct advantages and affecting the gasification process's efficiency and output. Air is the most common and cost-effective medium, producing lower-calorific-value syngas due to nitrogen dilution, making it ideal for small- to medium-scale applications where low-grade syngas can be used for heat and power generation. Oxygen, although more expensive due to the need for an oxygen supply system, produces higher-calorific-value syngas and is suitable for industrial applications requiring high-quality syngas for chemical production. Steam enhances the production of hydrogen-rich syngas and increases the endothermic reaction, requiring additional heat input, and is typically used for hydrogen production or in combined-cycle power generation systems. Carbon dioxide, while less common, can be used to reduce CO<sub>2</sub> emissions in specific gasification processes and helps control the reformation of carbon, making it useful in advanced gasification techniques for carbon capture and storage (CCS) strategies.

There are various types of gasifiers, each suited for different operational needs based on desired output, feedstock properties, and application requirements. Updraft (counter-current) gasifiers introduce air or oxygen at the bottom while fuel is fed from the top, producing syngas with higher tar content, suitable for low-moisture fuels. Downdraft (co-current) gasifiers allow air to enter at the top or sides, with fuel moving downward, producing low-tar syngas suitable for engines or turbines, commonly used in small- to medium-scale applications. Fluidized bed gasifiers suspend fuel in a bed of hot, fluidized particles, ensuring efficient mixing and uniform temperature distribution, resulting in higher conversion efficiency, suitable for large-scale, continuous operations with diverse feedstock options [6,7] Entrained flow gasifiers introduce finely ground fuel into the gasifier with oxygen or air at high velocity, operating at high temperatures to produce very low tar content and high-quality syngas, ideal for large-scale industrial applications with high demands for clean syngas.

A gasifier commonly comprises of a few particular zones, each assuming a particular part in the gasification cycle (Figure 1). The vital zones in a gasifier are:

> Drying Zone: In this zone, the feedstock is warmed to eliminate dampness. The kind of biomass utilized essentially decides the nature of the item in gasification. Consistently, biomass with a wet substance of 10% to 20% is recommended for conveying syngas with a high warming worth [8]. Highwet substance biomass requires drying in the drying zone before gasification. Regardless, the presence of high soddenness content prompts energy incident and taints the thing quality. The biomass' restricted water is changed over into steam north of 373 K, and this communication happen until 473 K.



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

> Pyrolysis Zone: The dry feedstock goes through pyrolysis in this zone, which is the power breakdown of normal particles without the presence of oxygen." The most precarious substance, hemicellulose, begins to crumble some place in the scope of 423 and 623 K, making tar, exhaust, and burn. A temperature of 573 K is sensible if consume improvement is the best outcome. Found in biomass, cellulose degrades at temperatures going from 548 to 623 K, conveying vaporous things, tar, and fire. Regardless, cellulose yields an in a general sense higher measure of tar when diverged from hemicellulose. Appeared differently in relation to cellulosic material, lignin creates more essential consume when it changes into aromatics from the lignocellulosic biomass. The temperature range in which lignin spoils is 523-773 K [9,10,11]. Subsequently, thing selectivity is by and large affected by the pyrolysis temperature. Critical tar is outlined more than 773 K, and the cycle conveys commonly vaporous things and bio-oils. As needs be, biomass pyrolysis occurs inside the extent of 398 to 773 K, causing the ascent of various things depending upon the picked temperature .This outcomes in the improvement of unstable mixes, including tars and gases.

 $\blacktriangleright$  Oxidation Zone: Here, a controlled proportion of oxygen is familiar with combust a piece of the pyrolysis things. This start reaction gives force to the overall gasification cycle and supports the significant high temperatures. In any case, appeared differently in relation to gasification, the general power set liberated from biomass constituents in the beginning zone is more unobtrusive. Exothermic material reactions happen inside the beginning zone, causing a temperature increase some place in the scope of 1373 and 1773 K [12,13]. The final products molded in this zone are CO, CO<sub>2</sub>, H<sub>2</sub>, and H<sub>2</sub>O. The power conveyed is used in the pyrolysis cycle and to dry the constituents somewhat.

➢ Reduction Zone: Remaining burn and any unburned pyrolysis things answer further with gases, for instance, carbon dioxide and water rage in the reduction zone. An excess of tar in the fuel gas cuts down biomass' overall adequacy and extends the plant's general bundle cost. Tar might conceivably hinder channels and even polymerize into tangled particles at whatever point left untreated. The most possible end-use circumstances for biomass gasification. The lower zone gets its name from its ability to reduce how much tar particles in the made gas. They are presented to a high temperature of roughly 1273 K to achieve this. [14]. Understanding and enhancing the circumstances in every one of these zones are significant for productive and powerful gasification. Legitimate control of temperature, home time, and gas arrangement in each zone adds to boosting the yield of attractive syngas and limiting undesirable side-effects.



Figure 1: Different zones in downdraft biomass gasifier [15]



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

# II CFD Methodology

## 2.1 CAD Model

A CAD model (Computer-Aided Design model) is a digital representation of an object or system created using specialized software. CAD models are used across various industries to design, simulate, and visualize components or structures before physical production or implementation. In the context of gasifiers, a CAD model can be created to represent the different zones, components, and geometry of the gasifier, allowing for detailed analysis, optimization, and design refinement. The feedstock was supplied to Ansys-Fluent using the coal calculator tool [16]. The CAD model provides a three-dimensional representation of the gasifier, including all distinct zones (e.g., drying, pyrolysis, combustion, reduction, and tar reforming zones). This visual detail helps in understanding how the gasifier's design influences the flow of gases, heat distribution, and material processing. It includes details like inlets for feedstock and air/oxygen, outlets for syngas, and internal structures like baffles, pipes, or grids to enhance mixing and reaction efficiency [17, 18]. The model can be used to assign material properties to different parts of the gasifier, enabling simulations of how materials will behave under high temperatures and chemical reactions within the gasifier environment.

A CAD model can be paired with simulations, such as those run using Computational Fluid Dynamics (CFD), to test various configurations of the gasifier and optimize it for better efficiency, syngas production, and operational stability. CAD models are critical for prototyping gasifiers as they provide the precise dimensions and assembly details required for fabrication. Manufacturers can use these models to produce the gasifier's components and ensure accurate construction. The model allows for easy modifications to test different design parameters, making it versatile for exploring the impact of scaling up or down the gasifier for different applications [19,20,21].

By leveraging CAD models, engineers can visualize complex systems like gasifiers and refine them for optimal performance before actual manufacturing or testing, saving time and costs in the development process. Figure 2 reports the two dimensional (2D) Computer Aided Drafting (CAD) model of the downdraft gasifier.



Figure 2: 2D CAD model of the downdraft gasifier

## 2.2 Operating parameter

#### 2.2.1 Gasification temperature

The gasification temperature refers to the range at which the gasification process occurs, typically between 700°C and 1600°C [22]. Different feedstocks require specific temperature ranges for effective conversion into syngas. For example, coal gasification generally operates at higher temperatures (1000°C–1600°C) to break down its solid structure and produce syngas rich in carbon monoxide (CO) and hydrogen (H<sub>2</sub>), while biomass gasification occurs at lower temperatures (700°C–1200°C) due to its lower ignition point[23,24]. The type of gasifier also significantly influences the operating temperature. Updraft gasifiers typically function at lower temperatures (700°C–1000°C), downdraft



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

gasifiers at intermediate temperatures (800°C–1200°C), fluidized bed gasifiers around 800°C to 1000°C, and entrained flow gasifiers at higher temperatures of 1200°C to 1600°C, ensuring rapid conversion and minimal tar production [25].

#### 2.2.2 Gasification pressure

Operating at elevated pressures generally increases the conversion efficiency of the gasification process, especially for coal and heavier feedstocks, and reduces the formation of undesirable by-products like tar [26]. However, high-pressure gasification systems come with challenges, requiring advanced equipment like compressors, pressure vessels, and safety mechanisms, which increases both the complexity and cost of the system.

#### 1.1.1 Biomass species

Biomass species refer to the diverse types of organic materials used in biomass energy production processes such as gasification, combustion, and fermentation. These species are categorized based on their source, composition, and suitability for energy conversion. Biomass species include plant, animal, and organic waste materials, which are renewable and widely available [27] Woody biomass such as trees, wood chips, and forestry residues is rich in lignin, cellulose, and hemicellulose, making it suitable for gasification and combustion. Common woody species include hardwoods like oak and eucalyptus, and softwoods like pine and spruce. Herbaceous biomass, including agricultural residues like straw and grasses such as switchgrass and miscanthus, is often used for bioenergy applications like bioethanol production due to its high cellulose content [28, 29, 30].

#### 2.2 Meshing

Meshing is a fundamental step in computational modelling and simulation, essential for accurately solving the governing equations in fields like Computational Fluid Dynamics (CFD) and Finite Element Analysis (FEA). The process involves dividing a complex geometric domain into smaller, manageable elements, which allows for the numerical approximation of differential equations governing fluid flow, heat transfer, and structural mechanics. Various mesh elements, such as tetrahedral for complex 3D geometries, hexahedral for simpler shapes, and prismatic/pyramidal for transitional regions, are used based on the specific needs of the simulation. Additionally, quadrilateral and triangle elements are commonly used in 2D simulations. CFD reference and familiar solver were utilized for network age. For the framework independency study, the mean size of components was decreased from 1.75 to 0.25 mm, with a 0.25 mm decrease in each step, as a multi-zone quadrilateral/triangle [31]. Overall, high-quality meshing is crucial for ensuring that simulations are accurate, efficient, and reliable, especially in complex processes like gasification. The meshing generated for the two dimensional (2D) model of the downdraft gasifier is reported in Figure 3.



Figure 3: Mesh Generated for 2 D model of the gasifier



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

## 2.3 Boundary condition

In a commercial modelling and simulation software, gasifier model would regularly include characterizing different limit conditions to address the actual way of behaving of the framework precisely [32]. Mass flow rate in the air inlet 1 and air inlet 2 is 0.205 kg/s at the initial gauge pressure 300000 pascal normal to the boundary where the total temperature is 441 K. On the wall surface body the mass flow rate is 0.0025 kg/s with same gauge pressure. In the outlet gauge pressure is 400000 pascal with 1000 K total backflow temperature. Walls of the gasifier are stationary with no slip shear condition.

## 2.4 Governing Equations

The governing equations in gasification include the continuity equation for mass conservation, the Navier-Stokes equations for momentum, the transfer, species transport equations for chemical species, chemical kinetics for reaction rates, and the ideal gas law for gas mixtures. These equations work together to simulate the complex interactions within a gasifier, including fluid flow, heat transfer, and chemical reactions, providing a comprehensive model of the gasification process [32].

Continuity equation (mass conservation) ensures that mass is conserved throughout the gasifier is  $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho u) = 0$ (1)

where 
$$\rho$$
 is the density of the fluid and u is the velocity vector.

$$\frac{\partial(\rho u)}{\partial t} + \nabla \cdot (\rho_{uu}) = -\nabla_p$$

Momentum equation (Navier-Stokes equations) describes the conservation of momentum for fluid flow, including both viscous and pressure forces is

$$\frac{\partial(\rho u)}{\partial t} + \nabla \cdot (\rho u u) = -\nabla_p + \nabla \cdot \left(\mu (\nabla u + (\nabla u)^T)\right) + f \tag{3}$$

where p is the pressure,  $\mu$  is the dynamic viscosity, and f represents body forces (e.g., gravity). Energy equation governs the thermal energy within the gasifier, accounting for conduction, convection, and potentially radiation is

$$\frac{\partial(\rho E)}{\partial t} + \nabla (\rho u E) = \nabla (k \nabla T) + \dot{Q}$$

where E is the total energy per unit mass, k is the thermal conductivity, T is the temperature, and  $\dot{Q}$  represents heat sources or sinks.

Species Transport Equations For modelling chemical reactions and tracking species concentrations (e.g., syngas components like CO, CO<sub>2</sub>, H<sub>2</sub>, and CH<sub>4</sub>) is

$$\frac{\partial(\rho Y_i)}{\partial t} + \nabla . \left(\rho u Y_i\right) = \nabla . \left(D_i \nabla Y_i\right) + \dot{\omega}_i$$

Where  $Y_i$  is the mass fraction of species i,  $D_i$  is the diffusion coefficient, and  $\dot{\omega}_i$  is the rate of production or consumption of species i due to chemical reactions.

In ANSYS Fluent or other CFD software, these equations are typically solved numerically using discretization methods. Boundary conditions and initial conditions must be defined based on the specific gasifier configuration and operating parameters.

## **III Results and Discussions**

For gasifier simulations, always consult the ANSYS manual and any special instructions given. Depending on the particular type of gasifier, the processes involved, and the specifics of the physical setup you are simulating, the precise boundary conditions may change. Table 1 shows the grid independency test results which refers to the point in a numerical simulation where further refinement of the computational grid no longer significantly affects the results of the simulation. Default mesh size is 0.023 m where we got the 400149.00 Pa pressure with 23.22 m/s velocity and 1444.67 K temperature. We'll choose scaling factors of 0.75x, 0.5x, and 0.25x the original size then it is observe that pressure, velocity and temperature decreases with decreasing mesh size. Where if we choose the scaling factors of 1.5x, 2x, and 4x the original size, it is observe that the value of pressure, velocity, temperature remains constant though the mesh size changes. At mesh size 0.0959 m results stabilize,

(2)

(4)

(5)





ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

and further refinement of the mesh no longer leads to noticeable changes where we obtain the grid independency stage. Table 1 Grid independency test results

S. No.	Mesh Size (m)	Pressure (Pa)	Velocity(m/s)	Temperature (K)
1.	0.01799	400130.91	20.35	2456.3
2.	0.01199	400127.03	20.53	1549.56
3.	0.005599	400140.00	21.18	1565.57
4.	0.023	400149.00	23.22	1444.67
5.	0.03598	400135.75	21.45	1782.6
6.	0.04797	400135.75	21.45	1782.6
7.	0.0959	400135.75	21.45	1782.6



Figure 4: Mesh analysis result for the gasifier model

Figure 4 shows the mesh analysis result with linear element order and 2.39 element size. ANSYS mesh analysis provides the foundation for reliable simulations by balancing mesh density, quality, and computational resources, ensuring accurate representation of the physical processes in gasifier systems [33,34].

Figure 5 shows Pressure distribution in different zones of the gasifier. Here, the inlet pressures can range from 400135.75 pa to 400118.78pa. In the outlet the pressure is around 400008.50pa. Pressure drop between the inlet and outlet is monitored to assess the efficiency of the process [35]. Pressure at the inlet of a gasifier is higher compared to the pressure at the outlet, this indicates a pressure drop within the gasifier. A moderate pressure drop is expected and indicates that the gas is flowing through the system and reacting with the biomass as intended. ANSYS CFD produces pressure contours that visually show pressure distribution in the gasifier. These contours are important for understanding where bottlenecks, flow disruptions, or pressure drops occur.



Figure 5: Pressure distribution in different zones of the gasifier

Figure 6 shows the velocity distribution in different zones of the gasifier. Inlet velocity is around 1.34m/s while outlet velocity is around 21.45m/s. As the gases pass through the gasifier, they are subjected to high temperatures due to the exothermic reactions. According to the ideal gas law, as the



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

temperature increases, the gas molecules move faster and expand. This expansion increases the volume of the gas, which in turn leads to an increase in the velocity at the outlet because the same mass of gas occupies a larger volume at the outlet compared to the inlet, where it was cooler. A higher outlet velocity may indicate that the gasification reactions are proceeding efficiently, producing a sufficient amount of syngas (a mixture of CO, H<sub>2</sub>, and CH<sub>4</sub>) and releasing the required energy for the process.



Figure 6: Velocity distribution in different zones of the gasifier.

Figure 7 shows the temperature distribution in different zones of the gasifier. Here, the drying zone, the temperature is 944.10 K. This zone is where moisture evaporates from the biomass feedstock. Here, the biomass begins to thermally decompose into gases, tars, and char. Simulations often highlight rapid temperature increases as volatile matter is released from the feedstock. The combustion zone, where partial oxidation occurs, shows temperature 1698 K. In the reduction zone, the remaining char reacts with  $CO_2$  and  $H_2O$  to form CO and  $H_2$  (syngas). The temperature in this zone is 1782.60 K. CFD analysis in ANSYS typically focuses on ensuring proper temperature control here to optimize syngas quality and minimize tar formation. The outlet temperature is 441 K. The highest temperatures are observed near the air inlet in the combustion zone, while gradual cooling occurs as the gases flow toward the outlet.



Figure 7: Temperature distribution in different zones of the gasifier.

#### **IV Conclusions**

The present work reported ANSYS CFD analysis of a downdraft gasifier. It provided critical insights into optimizing gasification processes, particularly in terms of temperature, pressure, and velocity

#### UGC CARE Group-1



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

distribution in different zones of the gasifier. These simulations are invaluable for improving the efficiency of syngas production, minimizing tar formation, and ensuring stable operation of gasifiers. With the current research pushing the boundaries of multi-phase flow and thermal management, downdraft gasifiers are becoming increasingly viable for clean energy production, especially in waste-to-energy scenarios. The future of gasification technology looks bright as it progresses toward enhanced fuel flexibility, lower environmental impact, and higher energy efficiency. Through advanced computational tools and experimental research, downdraft gasifiers could play a pivotal role in the shift towards sustainable energy solutions, particularly for decentralized energy production and waste management.

#### References

[1] Diego Mauricio Yepes Maya, Electo Eduardo Silva Lora, Rubenildo Vieira Andrade, Albert Ratner, Juan Daniel Martínez Angel 2021. Biomass gasification using mixtures of air, saturated steam, and oxygen in a two-stage downdraft gasifier. Assessment using a CFD modeling approach <a href="https://doi.org/10.1016/j.renene.2021.06.051">https://doi.org/10.1016/j.renene.2021.06.051</a>

[2] Rafael D. Gomez, Mario Palacio, Juan F. Arango, Adrian E. Avila, Jorge M. Mendoza. 2020. Evaluation of the energy generation potential by an experimental characterization of residual biomass blends from Córdoba, Colombia in a downdraft gasifier <u>https://doi.org/10.1016/j.wasman.2020.10.014</u>
[3] Bhoopendra Pandey, K. Yogesh Prajapati, N. Pratik Sheth 2020. Materials Today: Proceedings. <u>https://doi.org/10.1016/j.matpr.2020.10.451</u>

[4] Prashant Sharma, Bhupendra Gupta, Mukesh Pandey, Keshav Singh Bisen, Prashant Baredar. 2020. Downdraft biomass gasification: A review on concepts, designs analysis, modelling and recent advance <a href="https://doi.org/10.1016/j.matpr.2020.08.789">https://doi.org/10.1016/j.matpr.2020.08.789</a>

[5] Reza Jahromi, Mahdi Rezaei, Seyed Hashem Samadi, Hossein Jahromi. 2020. Biomass gasification in a downdraft fixed-bed gasifier: Optimization of operating conditions https://doi.org/10.1016/j.ces.2020.116249

[6] Caroline Smith Lewin, Ana Rosa Fonseca de Aguiar Martins and Florian Pradelle 2020. Modelling, simulation and optimization of a solid residues downdraft gasifier: Application to the cogasification of municipal solid waste and sugarcane bagasse https://doi.org/10.1016/j.energy.2020.118498

[7] Apri Wiyonoa , Nugroho Agung Pambudi B. Miftah Hijriawanb , Indra Mamad Gandidi a , Asep Setiadi Husena , Purnawan 2020 Dataset on the integrated downdraft gasifier and multi integrated gas cleaner system (IGCS) for municipal solid waste (MSW) https://doi.org/10.1016/j.dib.2020.105521

[8] Ashish Chaurasia 2020. Modeling of downdraft gasification process: Part II - Studies on the effect of shrinking and non-shrinking biomass geometries on the performance of gasification process https://doi.org/10.1016/j.energy.2020.118186

[9] S. A. Abdulrahman, A. T. Abdulrahim and A. M. El-Jummah 2019. COMBUSTION MODELING OF A FIXED BED DOWNDRAFT BIOMASS GASIFIER USING COMPUTATIONAL FLUID DYNAMICS DESIG <u>ARID ZONE JOURNAL OF ENGINEERING</u>, <u>TECHNOLOGY AND ENVIRONMENT (azojete.com.ng)</u>

[10] Umesh Kumar and Manosh C. Paul 2018. CFD modelling of biomass gasification with a volatile breakup approach <u>https://doi.org/10.1016/j.ces.2018.09.038</u>

[11] Randall Salazar Esquivel, Pedro Casanova Treto, Kattia Solís Ramírez 2018 Analysis of a downdraft gasifier for energy use of biomass waste applying computational fluid dynamics <u>IOSR</u> Journal (iosrjournals.org)

[12] João Silvaa, José Teixeirab, Senhorinha Teixeirac, Simone Preziatid, João Cassiano 2017 CFD Modeling of Combustion in Biomass Furnace <u>ScienceDirect.com</u> | <u>Science, health and medical</u> journals, full text articles and books.



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

[13] F. A. Atiku, A. R. Lea-Langton, K. D. Bartle, J. M. Jones, A. Williams, I. Burns,§ and G. Humphries 2022 Some Aspects of the Mechanism of Formation of Smoke from the Combustion of Wood <u>Some Aspects of the Mechanism of Formation of Smoke from the Combustion of Wood</u> <u>Energy & Fuels (acs.org)</u>

[14] Anil M1, Rupesh S1, Muraleedharan C1, Arun P 2016 Performance evaluation of fluidised bed biomass gasifier using CFD. <u>Sci-Hub | Performance Evaluation of Fluidised Bed Biomass Gasifier</u> Using CFD. Energy Procedia, 90, 154–162 | 10.1016/J.EGYPRO.2016.11.180

[15] https://www.researchgate.net/figure/Scheme-of-a-downdraft-gasifier\_fig1\_315922694

[16] Luc Gerun, Maria Paraschiv, Rãzvan Vîjeu, Jérôme Bellettre, Mohand Tazerout, Benny G øbel, Ulrik Henriksen 2017 Numerical investigation of the partial oxidation in a two-stage downdraft gasifier <u>Numerical investigation of the partial oxidation in a two-stage downdraft gasifier</u> - <u>ScienceDirect</u>

[17] M. Asadullah, Biomass gasification gas cleaning for downstream applications: a comparative critical review, Renew. Sustain. Energy Rev. 40 (2014) 118e132 https://doi.org/10.1016/j.rser.2014.07.132

[18] I.-S. Antonopoulos, A. Karagiannidis, A. Gkouletsos, G. Perkoulidis, Modelling of a downdraft gasifier fed by agricultural residues, Waste Manag. 32 (2012) 710e718, https://doi.org/10.1016/j.wasman.2011.12.015

[19] L. Gerun, M. Paraschiv, R. Vîjeu, J. Bellettre, M. Tazerout, B. Gøbel, U. Henriksen, Numerical investigation of the partial oxidation in a two-stage downdraft gasifier, Fuel 87 (2008) 1383e1393 https://doi.org/10.1016/j.fuel.2007.07.009

[20] Najafi, G., Ghobadian, B., Tavakoli, T., Yusaf, T., 2009. Potential of bioethanol production from agricultural wastes in Iran. Renewable and sustainable energy reviews 13, 1418-1427

[21] Reddy, M.V., Devi, M.P., Chandrasekhar, K., Goud, R.K., Mohan, S.V., 2011. Aerobic remediation of petroleum sludge through soil supplementation: microbial community analysis. Journal of hazardous materials 197, 80-87

[22] Ergun S. Fluid flow through packed columns. Chem Eng Prog 1952;48:89e94.

[23] Babu BV, Chaurasia AS. Modeling for pyrolysis of solid particle: kinetics and heat transfer effects. <u>https://doi.org/10.1016/S0196-8904(02)00252-2</u>

[24] Pyle DL, Zaror CA. Heat transfer and kinetics in the low temperature pyrolysis of solids. https://doi.org/10.1016/0009-2509(84)80140-2

[25] Jalan RK, Srivastava VK. Studies on pyrolysis of a single biomass cylindrical pellet- kinetic and heat transfer effects. <u>https://doi.org/10.1016/S0196-8904(98)00099-5</u>

[26] Bamford CH, Crank J, Malan DH. The combustion of wood. Part I. Proc Camb Phil Soc 1946;42:166e82.

[27] Numerical and Experimental Investigation of Equivalence Ratio (ER) and Feedstock Particle Size on Birchwood Gasification. Energies, 10(8), 1232. doi:10.3390/en10081232(2017).

[28] X. Hao, L. Guo, X. Zhang, Y. Guan, Hydrogen production from catalytic gasification of cellulose in supercritical water, Chem. Eng. J. 110 (1–3) (2005) 57–65, https://doi.org/10.1016/j.cej.2005.05.002

[29] Ahmad A, Zawawi N, Kasim F, Inayat A, Khasri A (2016) Assessing the gasification performance of biomass: a review on biomass gasification process conditions, optimization and economic evaluation. Renew Sust Energ Rev 53:1333–1347. https://doi.org/10.1016/j.rser.2015.09.030

[30] Baruah D, Baruah DC (2014) Modeling of biomass gasification: a review. Renew Sust Energ Rev 39:806–815. <u>https://doi.org/10.1016/j.rser.2014.07.129</u>

[31] Cardoso J, Silva V, Eusébio D, Brito P, Tarelho L (2018a) Improved numerical approaches to<br/>predict hydrodynamics in a pilot-scale bubbling fluidized bed biomass reactor: a numerical study with<br/>experimental validation. Energy Convers Manag 156:53–<br/>67. <a href="https://doi.org/10.1016/j.renene.2014.11.089">https://doi.org/10.1016/j.renene.2014.11.089</a>



ISSN: 0970-2555

Volume : 53, Issue 11, No.1, November : 2024

[32] ANSYS 15 Fluent Theory Guide, Canonsburg, PA 15317, 2013.

[33] Cardoso J, Silva VB, Eusébio D (2019b) Process optimization and robustness analysis of municipal solid waste gasification using air-carbon dioxide mixtures as gasifying agent. Int J Energy Res 43:4715–4728. <u>https://doi.org/10.1002/er.4611</u>

[34] Dinh CB, Liao CC, Hsiau SS (2017) Numerical study of hydrodynamics with surface heat transfer in a bubbling fluidized-bed reactor applied to fast pyrolysis of rice husk. Adv Powder Technol 28:419–429. <u>https://doi.org/10.1016/j.apt.2016.10.013</u>

[35] Fan H, Guo D, Dong J, Cui X, Zhang M, Zhang Z (2018) Discrete element method simulation of the mixing process of particles with and without cohesive interparticle forces in a fluidized bed. Powder Technol 327:223–231.

https://doi.org/10.1016/j.powtec.2017.12.016