

## Enhancement of CO<sub>2</sub>RR product formation on Cu-ZnO-based electrodes by varying ink formulation and post-treatment methods

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# Abstract

For the electrochemical CO2 reduction process, many catalysts have been described with better performance, such as extended lifespan and increased selectivity (CO2RR). Yet, very little is known about how the structure and pre-treatment of the electrodes affect this catalytic layer response. As a result, we describe in this article how changing the ink composition and applying an electrode treatment thereafter to the catalytic environment of a Cu-ZnO-carbon black catalyst before performing CO2RR. We also discuss the effects on the performance of the CO2RR of various solvents, ionomers, and additives used to prepare the ink as well as post-treatment activities like as pressing and sintering the produced electrodes. Although all electrodes having the same catalyst, there are notable variances in hydrophobicity, surface morphology,

### 1.Introduction

Tackling the negative effects of climate change requires new disruptive technologies. Along this line, the conversion of the greenhouse gas CO<sub>2</sub> into valuable chemicals is suggested to be key to achieve this goal [1]. A potential method to convert this molecule to e.g. multicarbon products is the use of surplus electricity from renewable energy sources to electrochemically drive this reduction. While the catalyst is key to facilitate the catalytic conversion of CO<sub>2</sub>, the electrode assembly and reactor setup play an equally important role to achieve efficient CO<sub>2</sub> reduction reaction (CO<sub>2</sub>RR) processes of industrial relevance. Along this line, a minimum current density of 200 mA cm<sup>-2</sup> with Faraday efficiencies (FEs) of at least 60% for multicarbon products are required [2–5]. Herein, utilization of gas diffusion electrodes (GDEs) in continuously driven flow cells showed promising results toward this aim. High achievable current densities and cell voltages below 3 V further support the promising role of GDEs for industrial CO<sub>2</sub>RR toward multicarbon products—e.g. Li *et al* reached a FE for ethanol of 41% at a partial current density of 250 mA cm<sup>-2</sup> using an Ag<sub>0.14</sub>/Cu<sub>0.86</sub> catalyst [6–10].

Among the large variety of reported catalysts, especially combinations of copper and zinc were shown to support the formation of C–C coupling products such as ethylene, ethanol, acetic acid, or propanol [11–13]



The C-C coupling was reported to follow a tandem mechanism with the Zn sites facilitating the CO<sub>2</sub> reduction to CO and the Cu sites allowing for subsequent CO coupling [14]. As of now, Cu seems to be essential for C-C bond formation and is currently the only metal electrocatalyst reported to enable this coupling step. However, many studies are limited to low current densities and with it low conversion rates. With respect to large-scale applications and the therein needed parameters, GDEs offer unique possibilities to adjust the three-phase boundary (TPB) at the catalyst by optimizing the interaction of CO<sub>2</sub>, catalyst, and water/protons and allow for efficient  $CO_2$  reduction at current densities >200 mA cm<sup>-2</sup>. This behavior is enabled by the efficient gas transport to the active sites of the catalyst, while simultaneously suppressing the parasitic hydrogen evolution reaction (HER). For example, Cu-ZnO-based GDEs allowed for FEs of up to 78% for  $C_{2+}$  products (mainly ethylene and ethanol) at potentials of 0.73 V and current densities of 466 mA cm<sup>-2</sup> [11]. Comparable high FEs of 60% C<sub>2</sub>H<sub>4</sub> and 25% EtOH [15] were reported for Cu-Ag based GDEs at -0.7 V with current densities of 180 mA cm<sup>-2</sup>. Additionally, B-Cu-Znbased GDEs were reported to form  $C_{2+}$  products with FEs of up to 79% [16].

In addition to the catalysts, the choice of process parameters during electrolysis was also shown to have a major influence on the product distribution and thus overall electrode performance. Especially the influence of the used electrolyte [17–19] alongside pH changes on the local environment, as well as the effects of temperature [20, 21] or pressure [22, 23] on the electrocatalytic performance and product distribution were reported as key factors. Beyond these process parameters and the choice of appropriate catalysts, Berlinguette, Schuhmann, as well as Apfel and coworkers recently showed the impact of electrode fabrication and composition itself on the overall product distribution by preparing various catalyst inks with different solvents in Cu- and Ag-GDEs [16, 24, 25].

The use of different solvents, carbon materials or even ionomer additives in the catalyst-containing ink accounted for significant differences in the observed FE in  $CO_2$  reduction to the various products formed. Especially, altered catalytic behavior utilizing different solvents occurred due to different agglomeration behavior of the ionomer that led to different microstructures of the catalyst layer. This change in return influences the  $CO_2RR$  product formation. Interestingly, similar observations were also made for fuel cell inks in the context of polymer electrolyte membrane fuel cells [26]. Additionally, the usage of ionomers like Nafion was reported to improve the electrolysis by contributing to a faster re-supply of  $CO_2$  and therefore increase the TPB formation where the  $CO_2RR$  takes place [27].

Furthermore, Chen and Su *et al* modulated the hydrophobicity within the catalyst layer of Cu-particle containing GDEs for the CO reduction using different amounts of polytetrafluoroethylene (PTFE). Increasing the binder content up to 25 wt.% increased the contact angle from 132.8° (5 wt.%) to 147.2° and led to higher  $C_{2+}$  product formation compared to 5 or 13 wt.%, probably due to enhanced CO supply at the catalyst [28]. Besides an increased supply of reactant gases, the increased hydrophobicity prevents the GDEs from flooding and stabilizes the electrodes during operation [27].

Additionally, the fabrication method influences the GDE's composition and therefore also the product distribution [29]. Along this line, Lees *et al* showed that airbrushed, drop-casted and ultrasonic spray coated electrodes revealed differences in their Nafion content distributions inside the catalyst layer accompanied by an overall altered CO<sub>2</sub>RR performance. These studies clearly show that research in electrocatalysis must not be exclusively focused on the catalyst systems but also on the application and modification of catalyst layers.

We herein further demonstrate the importance of the ink formulation and show that likewise UGC CARE Group-1, 485



post-treatment steps—like pressing and sintering of the sprayed electrode—have a significant effect on the GDEs' performance in  $CO_2RR$  processes. We believe that this opens a completely new space of parameters that must be understood with regard to the resulting physico-chemical properties and effects on GDEs foroptimized  $CO_2RR$ .

#### 2.Results and discussion

#### Experimental design strategy and electrode preparation

A carbon black (CB) supported copper–zinc catalyst was synthesized via an impregnation process (experimental part). The total anticipated metal loading on the CB support was 10 wt.% and the Cu:Zn mass ratio was adjusted to 85:15. Since promising results had already been obtained with impregnated CuCB catalysts [25], their impregnation process was adapted and extended to the additional use of Zn. This process includes partial surface oxidation of the CB, subsequent treatment with suitable metal salts and final reduction under H<sub>2</sub> atmosphere. In the current study, Zn was additionally added to facilitate the formation of  $C_{2+}$  products, especially alcohols. Notably, while the Cu:Zn ratio of 85:15 refers to the pure metal content, data from powder x-ray diffraction (figure S1) points toward the presence of a ZnO bulk material under the herein used conditions. In addition, inductively coupled plasma optical emission spectroscopy (ICP-OES) measurements reveal a slightly altered Cu:Zn ratio of 78.5:14.0 and a lower metal loading of 9.25 wt.% (instead of 10 wt.%) in the final electrode.







Figure 1 provides a general overview of the different ink compositions and post-treatment steps. A more detailed overview including a designation of the electrodes (IPA1–IPA5, Water1 and Water2) is given in table 1.

For all GDEs utilized in this study, the catalyst ink was deposited on a gas diffusion layer (GDL) by airbrushing. In addition to different ink compositions, the preparation method also includes subsequent pressing of the electrode to improve adhesion between the GDL and the catalyst layer as well as sintering to remove organic components by thermal decomposition. Pressing was conducted either at room temperature(RT) or at 130 °C. After pressing, the electrodes were partially sintered at 340 °C for 15 min in a muffle furnace under atmospheric conditions. Noteworthily, sintering also softens the PTFE and is thus supposed to increase its binding capabilities.

Notably, the same batches of catalyst and PTFE powder (3 M TF1750) were used for the catalyst layer preparation for all presented electrodes throughout this study. PTFE was selected as a binder material due to its hydrophobicity, known to increase the gas transport within the catalyst layer by minimizing pore flooding. Within this study, inks can be divided into two subgroups based on the solvent used to prepare the dispersions: those with (a) ethanol/water and (b) isopropanol. For the isopropanol-based inks (left strand in figure 1), we also investigated on how the usage of an additional anion exchange additive, the XA-9 ionomer, will alter the CO<sub>2</sub>RR activity of the GDE. Similarly, ink compositions based on ethanol/water mixtures were investigated (right strand in figure 1). Along this line, it is worth mentioning that Mowbray *et al* reported a higher FE<sub>CO</sub> during CO<sub>2</sub>RR for Ag-based GDEs when electrodes were sprayed with ethanol instead of propanol-based inks [24].

In addition to the catalyst, ethanol and water, Triton X-100 and 1 wt.% aqueous methyl cellulose solution were used as additional ink components. Triton X-100 as a non-ionic surfactant is expected to contribute to the formation of a stable ink dispersion during the air-brushing step and has been used before to modulate



Table 1. Overview of the composition of the various electrodes examined, including the associated post-treatment steps.

	Components	IPA1	IPA 1b	IPA2	IPA3	IPA4	IPA5	Water1	Water 1b	Water2	Water 2b
Solvent	Isopropanol	x	x	х	x	x	x				
	H <sub>2</sub> O/ethanol							х	х	х	x
Ink component (binder, pore former, surfactant, ionomer)	PTFE	х	х	х	х	х	х	х	х	х	x
	Methyl cellulose									х	x
	Triton							х		х	
	Sustainion XA-9 (ink)				x	x	x				
Post	Pressed (RT)					х	х				
treatment	Pressed (130 °C)		x	x				x	x	x	x
	Sintered (340 °C)			x				x	x	x	x
	Sustainion XA-9 layer	x	x	х			x	х	x	x	x



CO<sub>2</sub>RR [5, 30]. Methyl cellulose is used not only to thicken and stabilize the ink, but also to serve as a pore-forming agent in the catalyst layer [31].

The electrode preparation generally followed a standardized protocol: all ink components except the PTFE powder were dispersed under atmospheric conditions ( $5 \times 1$  min) using a high shear mixer/disperser (Ultraturrax) at about 300 W (13 800 rpm). Subsequently, the PTFE powder was added, and the process was repeated.

The thus produced ink was then airbrushed onto the GDL at 80 °C. Subsequent post-treatment steps such as pressing and sintering of the electrode were applied upon the spray coating process. For all electrodes, the total loading of the deposited layer, including catalyst and PTFE, was adjusted to 1 mg cm<sup>-2</sup>. Subsequently, round-shaped electrodes with a diameter of 22 mm were cut out, drop-casted with a Sustainion XA-9 solution and, after drying, immersed in 1 M KOH for at least 24 h.

This protocol was previously shown to lead to an optimal balance between the wetting of the electrode and the generation of  $C_{2+}$  products [25]. The ionomer XA-9 as an ion-conducting, hydrophilic ionomer is herein supposed to adjust the wetting properties of the catalyst layer and to suppress the flooding of the electrode by being a physical barrier toward the electrolyte solution. Notably, due to the lack of thermal stability of the SustainionXA-9 (figure S-2), these electrodes were only pressed at RT. Electrodes named with 'b' are repeats provided for comparison with an additional pressing step (electrode IPA1b) or leaving away Triton X (electrodes Water 1b and 2b). Their CO<sub>2</sub>RR results are shown in the SI section in figure S-8.

### **Physical properties of the GDEs**

### Ink formulation

Since spray coating usually requires a dispersion-stable ink where no agglomeration occurs at the relevant timescales of processing, it is essential to elucidate to what extent the inks will keep their initial consistency during the entire spraying process.

Thus, investigations on the stability of the inks were performed using an analytical centrifuge (figure S-2) [26]. Notably, only the ink for Water2 electrodes showed elevated stability for over 6 h at 400 rpm ( $\sim$ 21 × g (g-force)). Contrary, all other inks (IPA1/2, IPA3/4/5 and Water1) revealed fast sedimentation within a short time. Comparison with Water1b and Water2b inks produced without Triton shows no noticeable influence of Triton on the ink stability. For an improved understanding of the surface texture of the resulting catalyst layer and the CO<sub>2</sub>RR performance of the generated GDEs, the four inks, IPA1/2, IPA3/4/5, Water1, and Water2—all at identical solid concentration—were subsequently investigated by rheology (figure 2).

The flow curves of the inks for the preparation of electrodes IPA1/2, IPA3/4/5, and Water1 are almost identical, showing overall the same degree of shear thinning that can be ascribed to the breakup of CB agglomerates. This finding is in line with reports by Khandavalli *et al*, hypothesizing that weakly charged CB agglomerates form upon collisions induced by Brownian motion [32].

However, it can be anticipated that the microstructure of the catalyst layer is influenced by the properties of the inks, in particular by the degree of agglomeration during the coating step, but also by the interactions between the first layer of deposited particles and the substrate, as well as by particles inside the catalyst layer that come close and determine the structure formation upon drying. From the rheograms it becomes clear that only the inks for Water2 electrodes containing methyl cellulose revealed a Newtonian behavior. These findings suggest that these inks will behave differently during spraying and drying as compared to the other inks.





Table 2. Contact angle measurements of the electrodes with 1 M KOH before and after  $CO_2RR$  at 200 mA cm<sup>-2</sup> over 2 h (triple measurements) as well as crack density, carbonate formation and surface area (by N<sub>2</sub> sorption according to Brunauer–Emmett–Teller (BET). The evaluation in terms of crack density and carbonate formation is to be considered here as a relative assessment between the electrodes tested.

Electrode	Contact angle (before CO <sub>2</sub> RR)	Contact angle (after CO <sub>2</sub> RR)	Crack density (before CO <sub>2</sub> RR)	BET area (before CO <sub>2</sub> RR)	Carbonate formation (after CO <sub>2</sub> RR)
Water1	$153^{\circ} \pm 8^{\circ}$	$117^{\circ} \pm 12^{\circ}$	Low	$6.4 m_2^2 g_1^{-1}$	Severe
Water2	$159^{\circ} \pm 6^{\circ}$	$127^{\circ} \pm 8^{\circ}$	Medium	$8.2 \text{ m}^2 \text{ g}^{-1}$	Limited
IPA1	$150^{\circ} \pm 4^{\circ}$	$112^{\circ} \pm 22^{\circ}$	High	$7.9 \text{ m}^2 \text{ g}^{-1}$	Severe
IPA2	$162^{\circ} \pm 2^{\circ}$	$120^{\circ} \pm 11^{\circ}$	Low	$8.2 \text{ m}^2 \text{ g}^{-1}$	Severe
IPA3	$130^{\circ} \pm 19^{\circ}$	$109^{\circ} \pm 11^{\circ}$	High	$7.8 \text{ m}^2 \text{ g}^{-1}$	Limited
IPA4	$149^{\circ} \pm 7^{\circ}$	$95^{\circ} \pm 23^{\circ}$	High	$8.7 \text{ m}^2 \text{ g}^{-1}$	Limited
IPA5	$149^{\circ} \pm 7^{\circ}$	$103^{\circ} \pm 13^{\circ}$	Low	$8.7 \text{ m}^2 \text{ g}^{-1}$	Severe

### **As-prepared electrodes**

To further investigate the influence of the ink compositions, electrodes were prepared following the same procedure as described above. The electrodes and the surface properties of the obtained catalyst layers were then analyzed by scanning electron microscopy (SEM) measurements before and after electrolysis (figure 3). The gained results were related with the ink properties and the post-treatment procedure. Obviously, the ink formulation and the process conditions applied during catalyst layer preparation led to significant morphological differences in the surface structure, including both roughness and cracking.

Comparing the SEM images before  $CO_2RR$ , the highest surface roughness is found for electrode Water2, whose ink contained methyl cellulose and Triton. The surface of electrodes IPA2, IPA5, and electrode Water1 is smooth but nevertheless also shows some cracks. While electrode IPA1 reveals an uneven surface with pronounced crack formation (figure 3(a)), electrode IPA2 (figure 3(b)) displays a smooth surface morphology which seems to originate from levelling caused by pressing. Contrary, electrodes prepared without methyl cellulose (electrodes IPA2, IPA4, IPA5, and electrode Water1) showed an ultrathin detachment of the surface layer.

To further investigate the influence of the ink composition and electrode post-treatment on the surface properties of the electrodes, water contact angle measurements were carried out on the assembled electrodes before CO<sub>2</sub>RR and without application of a Sustainion XA-9 layer (table 2). The reason for not



applying the XA-9 layer for the contact angle measurements is that this topping layer would significantly interfere with the measurements due to its hydrophilicity. Hence, the presence of Sustainion XA-9 would prevent the gain of meaningful information about the catalyst layer itself. It can be seen, that for electrodes IPA1 and IPA2 as well as for IPA3 and IPA4, the presence of pressing leads to an increase in the contact angle.

The more even surfaces resulting from pressing, i.e. comparing electrodes IPA1 and IPA2 (figures 3(a) and (b)), lead to higher water contact angles and thus increased hydrophobicity. Interestingly, the contact angles of the electrodes Water1 and Water2 are very close to each other despite the large differences in their surface morphology (figures 3(d) and (e)).

In contrast, water sorption measurements show an altered trend with a higher hydrophobicity for electrode Water1 compared to electrode Water2. Overall, electrodes IPA3, IPA4 and electrode IPA5, with









carbonate crystals.



Sustainion XA-9 directly added to the ink formulation, generally had the lowest contact angles in the tested series. This is in line with our expectations, since Sustainion XA-9 is supposed to increase the wettability of the electrode due to its hydrophilic character.

Water sorption measurements (figure 4(d)) also revealed that the bulk hydrophobicity is lower for the pressed electrodes, i.e. electrode IPA2 vs. electrode IPA1 and electrode IPA4 vs. electrode IPA3.

However, only three of the four pressed electrodes, electrode Water2, electrode IPA2 and electrode IPA4 show a reduced hydrophobicity with Sustainion XA-9 after CO<sub>2</sub>RR. The other electrodes, electrode Water1, electrode IPA1, and electrode IPA3 nearly end up with the same value of around 0.36-0.38 cm<sup>-3</sup> m<sup>-2</sup>.

Interestingly, the electrodes Water2, IPA2, and IPA4 show a two-step water sorption process. This behavior can be explained by larger and more hydrophilic pores that fill up with water first, followed by filling the smaller ones. In general, it is notable that the observed trends for contact angle measurements and the bulk hydrophobicity determined via water physisorption are opposite. This shows that surface and bulk properties can differ significantly because of, e.g. surface roughness or different porous structures within the catalyst layer. Thus, the analysis of the surface structure/morphology is not sufficient to allow for a reliable judgement of the electrode composition and setting up structure/activity relationships but must be accompanied by additional methods that give access to the pore network inside the catalyst layer.

In addition, the bulk properties of the GDEs were also determined using nitrogen physisorption measurements (figure 4). All isotherms obtained from the N<sub>2</sub> sorption measurements were evaluated according to the BET method and belong to type II isotherms, i.e. showing a multilayer adsorption. Type II isotherms are typical for non-porous or macroporous substrates with pore diameters above 50 nm. As all isotherms show a rather flat instead of a sharp increase at low pressures, an overlap of the monolayer formation and the multilayer adsorption is anticipated. Especially for electrode Water1 and electrode IPA4, hysteresis loops are visible, which can be associated with capillary condensation [33]. In addition, N<sub>2</sub> sorption measurements (figures 4(a)–(c)) reveal highest surface areas for electrode IPA4 (8.7 m<sup>2</sup> g<sup>-1</sup>) as compared to electrode IPA2 (8.2 m<sup>2</sup> g<sup>-1</sup>) and electrode Water2 (8.2 m<sup>2</sup> g<sup>-1</sup>). Overall, the following BET surfaces were obtained: 6.4 m<sup>2</sup> g<sup>-1</sup> (electrode Water1), 7.8 m<sup>2</sup> g<sup>-1</sup>(electrode IPA3), 7.9 m<sup>2</sup> g<sup>-1</sup> (electrode IPA1), 8.2 m<sup>2</sup> g<sup>-1</sup> (electrode IPA2), 8.2 m<sup>2</sup> g<sup>-1</sup> (electrode Water2) and 8.7 m<sup>2</sup> g<sup>-1</sup> (electrode IPA4).

As it is noted, no clear trend can be deduced from the ink composition and micro structuring of the surfaces linking them with the BET results. This already points toward hidden parameters that must be unraveled in a targeted way in future studies. A major difference to all other electrodes is observed for the surface of electrode Water1, which finally manifests by the results of N<sub>2</sub> sorption, revealing a minimum value for the specific surface area of 6.4 m<sup>2</sup> g<sup>-1</sup>.

### **Electrodes after electro catalysis**

The comparison of the surface morphologies of the electrodes before and after  $CO_2RR$  at 200 mA cm<sup>-2</sup> shows that the surfaces generally exhibit more cracks after electrolysis. Only when methyl cellulose containing inks were used, as in case of electrode Water2 (figure 3(e)), fewer cracks were observed, suggesting a beneficial pore structuring. It is possible that cracks in the catalyst layer support the flooding behavior, since the electrolyte can penetrate more easily into the GDE [34].

Along this line, Kong *et al* compared the CO<sub>2</sub>RR of Ag nanoparticles using two different GDLs based on carbon paper. The first GDL using carbon paper from Freudenberg as macroporous layer (MPL) showed a lot of cracks, whereas when carbon paper from Sigracet was used as MPL, a compact and dense surface



was obtained. The performance of the Freudenberg electrode was superior during electrosynthesis and showed an elevated stability due to the direct access of the electrolyte solution to the carbon fiber network. The facilitated access resulted in an enhanced carbonate formation within the fibers instead of blocking the active sites of the catalyst. The authors concluded, that cracks within GDLs can be beneficial for the overall water management [35]. The carbonate precipitation occurs due to the simultaneous presence of  $CO_2$  and  $OH^-$  during  $CO_2RR$  resulting in the growth of carbonate crystals within the catalytic layer as well as the GDL. In this work, carbonate formation was in particular observed for electrodes IPA1, IPA2, IPA5 and electrode Water1, which showed large areas of the electrode surface (top view) populated with crystals (figures 3(a)–(d) and S-5). In addition, the elemental mapping (figure S-6) showed mainly the presence of potassium and oxygen, but also of copper as rod-shaped crystals. Especially, the needle-shaped copper crystals suggest catalyst leaching during  $CO_2RR$  (figure S-6).

Even after CO<sub>2</sub>RR, the electrode Water2 (figure 3(e)) showed the most uneven surface and the most cavities. Here, carbonate crystals can also be seen (red arrow) that mostly appear as narrow rods. In contrast and as mentioned before, electrodes produced without methyl cellulose in the ink formulation (figures 3(a)–(d)), showed larger and more cracks and furthermore revealed larger crystals spread out over a large area. SEM-energy dispersive x-ray spectroscopy (EDX) investigations of the electrode surfaces clearly indicate that the crystals consist of potassium carbonate (figure S-5). Notably, electrodes prepared from inks formulated without methyl cellulose showed a relatively uniform crack formation (figure S-5). This could be caused by the damage of the catalytic layer during the electrocatalytic processes, but also due to damage during the subsequent drying of the wetted catalyst layer.

Since EDX measurements showed no zinc after the CO<sub>2</sub>RR experiments, a leaching out of the metal during the electrochemical measurements is anticipated. At this point it has to be mentioned that, unfortunately, ICP-OES analysis after CO<sub>2</sub>RR is hard to realize for the following reasons:

After  $CO_2RR$  additionally to the pure catalyst, PTFE and Sustainion XA-9 are present and therefore need to be separated from the measurement data to assure correct results.

(a) As can be seen from the SEM micrographs, there is an irregular carbonate formation at the catalyst layer, which also falsifies the results.

(b) For an analysis after  $CO_2RR$ , the catalyst layer would have to be scraped off the GDL which is hardly doable. The result could be falsified by the separating parts of the microporous layer.

Likewise, ICP-OES analyses of the catholyte solution could not confirm leaching, as no zinc (or copper) was detectable. This points toward a small but continuous dissolution over time into the electrolyte. In addition, although EDX measurements of the electrodes before  $CO_2RR$  clearly revealed the presence of Zn(figure S-7), the addition of Sustainion XA-9 before electrocatalysis as well as the formation of

potassium-containing crystals on the surface can interfere with the detection of Zn in deeper layers and thus falsify this result. This observation confirms that complicated electrocatalysts can easily dealloy or restructure at higher current densities and thus will eventually provide an altered product spectrum for CO<sub>2</sub>RR during aging.

Overall, a decrease in contact angles and thus surface hydrophobicity was observed for all electrodes after



electrolysis. This decrease is not only due to the application of the hydrophilic Sustainion XA-9 top layer. This becomes clear from the electrodes IPA3 and IPA4 as there was no Sustainion XA-9 layer applied before CO<sub>2</sub>RR. For those electrodes, the contact angles were significantly smaller and even reached some of the lowest values after electrolysis with a decrease from 130° to 109° and 149° to 95°, respectively. The loss in hydrophobicity during the CO<sub>2</sub>RR measurement has repeatedly been described in the literature and can be attributed to several phenomena: (a) degradation of PTFE, (b) erosion of the catalytic layer, (c) formation of carbonates within the GDE, (d) increasing oxygen coverage of carbon surfaces [30, 36, 37]. The largest contact angle is obtained for the electrode Water2 (127°), which was produced with methyl cellulose as a pore forming agent alongside EtOH/H<sub>2</sub>O as solvent. Likewise, the SEM (-EDX) images (figures 3 and S-5, S-6) show that hygroscopic potassium salts formed on the electrode surface, which additionally leads to smaller contact angle measurements after CO<sub>2</sub>RR, since the obtained value heavily depends on the morphology of the electrode surface below the 1 M KOH droplet.

Changes in the surface morphology due to salt and crack formation were observed and were the smallest for electrode Water2. These small deviations in the hydrophobicity are also mirrored in the tested electrode itself and increase the overall stability of the electrode during electrolysis.

In general, effective  $CO_2RR$  gas-water pathways within the catalyst layer, created by hydrophobic additives like PTFE, are necessary to ensure  $CO_2$  and product transport [30]. Furthermore, the roughness and morphology of the surface of the catalyst layer (top view) strongly influence the hydrophobic behavior of the surroundings. Hence, with enhanced roughness, surfaces showed an increased hydrophobicity.

### **Electrochemical characterization**

Investigations on the electrochemical  $CO_2RR$  were performed by chronopotentiometric measurements, where electrodes were placed into an electrochemical flow cell (figure S-4). In brief, the catalyst layer faces the 1 M KOH electrolyte solution, while the GDL faces the gas compartment where  $CO_2$  is supplied. All electrochemical measurements were performed over 2 h at 200 mA cm<sup>-2</sup> at RT.

The electrolyte solution was circulated through the cathode and anode chamber, respectively, to prevent a partial temperature increase, to transport formed products away from the electrodes, and to provide fresh electrolyte to the electrode surface. As the objective is to increase the  $FE_{C2+}$ , especially ethanol and ethylene, the scope of the following discussion is focused mainly on these products.

To determine the stability of the utilized electrodes and their selectivity for  $C_{2+}$  products, gas samples were collected every 20 min over the course of 2 h by a coupled online gas chromatography-mass spectrometry (GC-MS) system with liquid analysis being performed after the electrolysis. In addition to the different surface morphologies and hydrophilicities, the  $CO_2$  reduction itself is strongly influenced by the chosen process chain, i.e. the composition of the different inks used for the preparation of the different catalyst layers and the subsequent post-treatments of the generated electrodes. The total FEs resulting from the 2 h electrolysis for the different electrodes are shown in figure 5(a).

By changing the ink composition as well as the post treatment of the electrodes, the FE for the  $CO_2RR$  can be heavily altered. Specifically, for the formation of ethanol, an increase from 0% (electrode IPA3 and



electrode IPA4) up to 11.2% for electrode Water2 can be achieved and is in line with the larger contact angles (table 2) and thus higher surface hydrophobicity.

In addition, SEM images showed significantly fewer cracks for electrode Water2 than for the others and also the formation of fewer crystals covering larger areas (figures 3 and S-5). For electrode Water2,  $C_{2+}$ 





products with an average FE of 39.5% were observed. In general, figure 5(a) shows, with regard to electrodes IPA1 and IPA2, that pressing and sintering of the electrode indeed has a significant effect on the surface morphology (figures 3(a) and (b)) as well as on the FEs of CO<sub>2</sub>RR products. For electrode IPA1, a noticeable gas formation at the GDE toward the cathode electrolyte compartment was visible during electrolysis. Since KOH is used as the electrolyte, the product gas stream cannot be passed over the catholyte again to also analyze the product gases there. This would directly lead to the formation of carbonates. Therefore, the catholyte gas space was not analyzed in this setup. The total FE reached was under 53%, but nevertheless, theFE for ethanol was 4.8% for electrode IPA1. The electrode IPA2 was sprayed using the same ink as in the case of electrode IPA1, but additionally, it has been post-pressed and sintered. These post-treatment steps, which also levelled the surface of the therewith generated electrodes (figures 3(a) and (b)), seem to have stabilized the electrodes' performance, giving overall FEs of almost 90%. In addition, a shift in the product spectrum can be observed for electrode IPA2 as the formation of CO is lower than in case of electrode IPA1 and an increase in methane and ethylene formation occurred. Notably, the FE<sub>CO</sub> increased from 3.2% (electrode IPA1) to 14% (electrode IPA2), while the FE of CH<sub>4</sub> increased



from 3.1% to 5.6% and the FE for ethylene even from 4.7% to 14.2%. Combining these observations with the earlier findings on contact angles (table 2), it becomes clear that the increased formation of  $CO_2RR$  products correlates with a higher hydrophobicity of the surface for the electrode. We suggest to take this as a first design rule for  $CO_2RR$  electrode manufacturing. Control experiments with the electrode IPA1b showed that pressing has a stabilizing effect on the electrode performance and higher FEs are achieved for products like ethylene in comparison to electrode IPA1 (5.2% vs. 4.7%) as well as methane (7.6% vs. 3.1%) and ethanol (5.7% vs. 4.8%). However, the FEs for the  $CO_2RR$  products increase further with the additional sintering of electrode IPA2. Probably, as a result of the sintering process at 340 °C, oxidation of the copper occurred. It is known from the literature that the reduction of copper oxides under the  $CO_2RR$  conditions and the resulting defects and grainboundaries may increase the surface activity [13].

The post-treatment of electrode IPA2 led to higher contact angles of 162° (before) and 120° (after electrolysis) compared to electrode IPA1 with 150° and 112°, respectively. However, there was a slight decrease in the FE for ethanol, which dropped from 4.8% to 4.2%. Nevertheless, among all the electrodes presented here, electrode IPA2 showed the highest formation of formic acid of 11.2%. Comparison of the Sustainion containing electrodes IPA3 and IPA4 exhibited strong gas evolution toward the cathode compartment and in addition, on-line GC-MS analysis showed hydrogen being the main product.

Post-pressing seems to have a minimal effect on the gas evolution toward the cathode compartment. Total FEs were obtained for electrode IPA4 of about 40% in contrast to about 35% for electrode IPA3, with the total FE toward CO<sub>2</sub>RR products being <1.6% in either case. Although the presence of post-treatment again resulted in higher hydrophobicity for electrode IPA2 in contrast to IPA1 (table 2), no increased formation of CO<sub>2</sub>RR products was observed. Drop casting with Sustainion XA-9 improved this behavior considerably.

With electrode IPA5 ethanol FEs of 5.1% were achieved while the rest of the  $CO_2RR$  spectrum comprised ethylene (FE 4.5%), CO (FE 8.3%) and CH<sub>4</sub> (FE 7.0%).

As noted, the best CO<sub>2</sub>RR results were obtained with electrodes made from EtOH/H<sub>2</sub>O-based inks, i.e. electrode Water1 and electrode Water2. In addition, the effect of Triton (for electrode Water1) and Triton/methyl cellulose (for electrode Water2) was investigated. Both, electrodes Water1 and Water2 showed the best CO<sub>2</sub>RR results among all tested electrodes, with FEs of 9.3% and 11.2% for ethanol and 13.5% and 23.7% for ethylene, respectively. Interestingly, FEs of 2.2% and 2.7% for acetic acid and 0.7% and 1.8% for propanol were achieved for electrodes Water1 and Water2, respectively. Particularly striking is the relatively high value for the formation of methane at electrode Water1, with 6.7%. Likewise, electrode Water2 showed a very high yield for CO<sub>2</sub>RR products in general, which has been accompanied by low FEs for the HER of solely 30%. Control electrodes prepared without Triton (electrodes Water1 and Water2), figure S-8) in the ink showed a lower formation of C<sub>2+</sub> products than the electrodes Water1 and Water2. FE<sub>EtOH</sub> of 9% and FE<sub>ethylene</sub> of 7% were achieved for electrode Water1b, 10% and 19% for electrode Water2b, respectively. Along this line, it has been shown previously for pure Cu-GDEs, that varying the ink composition, as by changing the solvent, has an effect on the microstructuring of the GDE. The reason is that the used solvent affects how binders and catalyst particles interact with each other [34].

In figures 5(b) and (c) the composition of gas products over the course of the 2 h experiment is shown, with the gas stream examined every 20 min by online GC-MS. In addition, the averaged course of the chronopotentiometry curves from the  $CO_2RR$  for the different electrodes is displayed. For the chronopotentiometry curves, a change in voltage towards more positive values can be associated with flooding of the GDE [38]. During the flooding, the diffusion paths of the  $CO_2$  are blocked by carbonate formation in the electrode. When the electrolyte solution has penetrated the entire electrode, the transport



of CO<sub>2</sub> toward the catalyst surface is limited by its solubility in the electrolyte. Due to the wetting of more electrode surface with the electrolyte solution, a higher active area is obtained, resulting in a more positive potential. In these cases, consequently, a significant increase in H<sub>2</sub> formation is also observed, while the CO<sub>2</sub>RR decreases. A very significant increase in voltage can be observed for the electrodes IPA1, IPA3, IPA4, and electrode IPA5 (figures 5(b) and (c)). The increase in voltage over time suggests that in addition to the mentioned observations from literature, the presence of cracks may not only increase the mass transport but also promote flooding of the electrode. Furthermore, a visibly stronger gas evolution toward the cathode chamber was observed, which probably constitutes of mainly hydrogen formation. Especially for electrode IPA5, but also for the other two electrodes IPA3 and IPA4 with Sustainion XA-9 in the bulk, a decrease of the CO<sub>2</sub>RR product formation over time is noticeable. The lower CO<sub>2</sub>RR for electrodes IPA1-5 and Water1 compared to electrode Water2 is accompanied by the increased formation of carbonates on top and inside the catalyst layer, as discussed previously (figures 3 and S-5).

The comparison of electrodes IPA3, IPA4, and IPA5 also shows the influence of the coating of the electrode with a Sustainion XA-9 layer. In the case of electrode IPA5, the additional layer results in a flatter chronopotentiometry curve which indicates a significantly more inhibited flooding behavior. In addition, similar to our previous results on Cu-GDEs, the Sustainion XA-9 layer optimizes the local environment and wetting of the electrode, significantly favoring the CO<sub>2</sub>RR [25]. With regard to electrode IPA1, it is also apparent from both the course of the chronopotentiometry curve and the gas product distribution, that post-treatment of the electrode by means of pressing and sintering (electrode IPA2 vs. electrode IPA1) can significantly improve the overall CO<sub>2</sub>RR performance. The resulting potential curve for electrode IPA2 shows a more stable behavior and the potential remains at an approximately constant level in the range of

-2.6 to -2.7 V (not iR corrected) during the 2 h period. As previously discussed, this behavior indicates a decreased tendency of the electrode towards flooding. This is simultaneously associated with an elevated production of CO<sub>2</sub>RR products, especially C<sub>2+</sub>, over time. Nevertheless, for electrode IPA2 a decrease of the CO<sub>2</sub>RR product formation is noticeable, such as ethylene with a FE of 18.8% after 20 min to 11.2% after 2 h with a simultaneous increase of H<sub>2</sub> formation from 33.5% to 53.8%. Thus, a progressive flooding occurs within the duration of the experiment of 2 h.

As the thickness of the catalyst layer is known to affect the local concentration of CO<sub>2</sub> and therefore the CO<sub>2</sub>RR product distribution, the thickness of the catalyst layer of electrode Water2 was systematically varied (figure S-9). This was realized by adding additional layers of catalyst and thus also achieving a varying catalyst loading of 0.5, 1, and 1.3 mg cm<sup>-2</sup>. At 0.5 mg cm<sup>-2</sup> (the thinnest electrode), the lowest FEs for CO<sub>2</sub>RR were observed. Moreover, the passage of CO<sub>2</sub> through the GDE into the catholyte occurred. The overall yield of C<sub>2+</sub> products was approximately 13%. At 1.3 mg cm<sup>-2</sup> (the thickest electrode), a drop in CO<sub>2</sub>RR products in favor of HER was observable. The overall FE of C<sub>2+</sub> products decreased from about 40%–33%.

Regarding the long-term stability of the EtOH/H<sub>2</sub>O electrodes (electrodes Water1 and Water2), a generally higher H<sub>2</sub> production as electrolysis progresses is observed. In contrast, electrode Water2 showed a stable potential curve (at about -2.7 V) without any voltage increase. In addition, the hydrogen formation remained clearly more constant over time and always ranged between 24.3% and 33.5%. The formation of the CO<sub>2</sub>RR products showed a slight increase in CH<sub>4</sub> formation from 2.4% to 3.5%, while at the same time the FE<sub>CO</sub> decreases slightly from 11.7% to 9.4%. The FE for ethylene was in the range of 23%–26.4%. The electrode Water2 showed both the best FEs for CO<sub>2</sub>RR products and, according to the SEM images, the uneven surface with the most pores (figure 3(e)). In addition, the contact angles after electrolysis of 127° showed that in comparison to other electrodes, the electrode Water2 experiences a decreased loss in



hydrophobicity over the measurement period of 2 h compared to other electrodes (see table 2). In addition, the SEM images after electrolysis showed significantly fewer crystals and cracks than in case of all other electrodes of this study.

### **Implications for electrode assemblies**

In terms of electrochemical performance, the comparison of the isopropanol and water/ethanol-based inks shows that for the latter higher FEs were obtained for  $CO_2RR$  products. These higher FEs occur although no notable trends with respect to BET surface areas or hydrophobicity emerge.

Furthermore, the observed morphology differences suggest that the absence of methyl cellulose as pore forming agent leads to an overall smoother surface as is visible when comparing electrode Water1 (d) and electrode Water2 (e) in figure 3. The use of methyl cellulose as pore-forming agent stabilized the ink decisively and at the same time resulted in an increased BET surface area and a much rougher surface.

During  $CO_2RR$ , the usage of the electrode made from an ink containing methyl cellulose also exhibited the lowest flooding behavior and resulted in the highest yield of  $C_{2+}$  products, particularly EtOH and ethylene.

Addition of Sustainion XA-9 as well as Triton X-100 to the ink had no significant influence on the surface texture (top view). The addition of Sustainion XA-9 generally resulted in a more hydrophilic surface (contact angle measurements), but led to a more hydrophobic bulk material. It is possible that the added ionomer herein alters the pore structure inside the catalyst layer (CL), resulting in the altered hydrophobicity. The addition of Sustainion XA-9 also led to faster flooding of the electrode and reduced formation of  $CO_2RR$  products, particularly  $C_{2+}$ , probably due to the lower hydrophobicity of the electrode. The usage of Triton had no impact on ink stability, however, electrodes Water1b and Water2b (without Triton) showed less  $C_{2+}$  product formation and higher HER in comparison to electrodes containing Triton. Herein, the addition of Triton might have influenced the microstructuring of the electrodes with Sustainion XA-9 prior to  $CO_2RR$  has a crucial influence. As described by Junge Puring *et al*, this provides an additional barrier that reduces electrode flooding and increases the  $CO_2RR$  production [25].

Concerning post-treatment of the electrodes, it is visible that the absence of a sintering step results in higher BET surfaces as is notable for electrode IPA5. Herein, the temperature is not high enough to allow for the decomposition of Sustainion XA-9 which was subsequently supported by TG-DTA measurements (thermogravimetric analysis—differential thermal analysis, figure S-3). Still sintering seems to have a less significant effect on the physical properties of the electrodes in the absence of methyl cellulose. The comparison of electrodes IPA1, IPA1b and IPA2 shows a stabilization due to the post-pressing, but largest differences are observed due to the sintering process, which results in a significant increase of CO<sub>2</sub>RR products, especially ethylene. For post-pressed electrodes, a potential stabilization was observed and less gas was released into the cathode compartment during electrolysis with higher FEs for CO<sub>2</sub>RR products. At both elevated and RT pressing methods, a significant levelling was observed for the surface of the catalyst layer. This becomes clear from the flatter surface morphology and larger BET surface area that were obtained for the non-sintered electrode pressed only at RT.

### 2. Conclusion

In this work, CO<sub>2</sub>RR was performed using Cu-ZnO-CB GDEs manufactured from different inks and utilizing pressing and sintering as post-treatment methods. Herein we show that solvents used to prepare the catalyst inks will eventually lead to an alteration of the electrode structure and morphology equally as the use of additional additives like pore forming agents or ionomers. Likewise, post-treatment of the freshly



prepared electrodes, namely pressing and sintering in comparison with unprocessed electrodes was evaluated.

We show that these post-treatment strategies are equally important than the ink formulation and the catalyst to achieve a certain performance. In summary, the best results were obtained when catalyst layers were spray coated with inks based upon a water-ethanol based solvent mixture and in the presence of additives that were able to establish proper pore structures, i.e. pore-forming agents. Especially, electrodes post-treated by hot pressing methods showed a higher surface hydrophobicity after CO<sub>2</sub>RR and also displayed higher CO<sub>2</sub>RR activity along with higher C<sub>2+</sub> product formation compared to GDEs without post treatment. Thus, under the herein presented experimental conditions, a stable CO<sub>2</sub>RR performance with FEs for ethanol and ethylene of up to 11.2% and 23.7%, respectively, at 200 mA cm<sup>-2</sup> was obtained. Yet, lowering the flooding behavior and therefore HER is still a critical issue that needs to be resolved in the future.

In summary, we herein show that the ink composition and post-treatment of GDEs have a significant impact on the stability and electrochemical performance of GDEs. Deciphering these manifold influencing factors in a multidimensional parameter space requires coherent workflows and detailed, highly systematic studies. This will be established and discussed in the near future.



### 3. Experimental section

#### Materials

Copper(II)acetate hydrate (98%, Alfa Aesar), zinc(II)acetate dihydrate ( $\geq$ 99%, VWR), ENSACO 250 G CB (Imery's Graphite & Carbon), DyneonTM PTFE Powder TF 1750 (3 M) and KOH (p.a., Merck) were used as received from the commercial vendors. Furthermore, Sustainion XA-9 Alkaline Ionomer 5% in ethanol (Dioxide Materials) and Carbon Cloth GDLs with MPL (W1S1011, FuelCellStore) were used for electrode preparation.

#### **Catalyst synthesis**

The catalyst synthesis was carried out according to a procedure described by the following literature reports [25]. To receive 10% metal loading related to CB, Cu(II)- and Zn(II)-acetate (mass ratio Cu: Zn 85:15) were dissolved in 500 ml deionized water. Subsequently, 9 g CB was added, and the suspension was sonicated for 3 h. Then, the water was removed via rotary evaporation and the resulting precursor was dried overnight at 105 °C and mortared. The precursor powder was placed between glass wool within a glass reactor in a tubular furnace, flushed with N<sub>2</sub> for 10 min at RT and afterwards reduced in H<sub>2</sub> atmosphere at 250 °C for 5 h. Cooling to RT was then carried out again under N<sub>2</sub> flushing.

#### **Electrode preparation**

The impregnated CB catalyst was processed into different inks. In a representative example, 0.5 g of the catalyst was used, and 30 ml isopropanol was weighed in centrifuge tubes (50 ml) and mixed via a shear mixer/disperser (IKA T18 digital Ultra TURRAX) (five times for 1 min at 13.800 rpm, 1 min pause).

Subsequently, 0.055 g PTFE powder was added and mixing (five times for 1 min at 13.800 rpm) was repeated.

The process for making each of the inks followed the principle that first, everything except PTFE was weighed in, mixed, and afterwards PTFE was added. Then, the mixing process was repeated using the Ultraturrax. For the electrodes containing Sustainion XA-9 in bulk, 133  $\mu$ l were added to the ink (besides isopropanol, catalyst, and PTFE). The EtOH/H<sub>2</sub>O-based inks consisted of 0.5 g catalyst, 5.4 ml MilliQ water, 15 ml ethanol, 0.15 g Triton X 100 and 10 g 1 wt.% aqueous methyl cellulose solution as well as 0.55 g PTFE powder. In case of EtOH/H2O-based inks without methyl cellulose solution, 15 ml MilliQ were used. All inkswere airbrushed using an Iwata-Eclipse airbrush pistol and a nitrogen pressure of 1 bar onto 10 cm<sup>2</sup> carbon cloth, which was heated to 80 °C. The electrodes were repeatedly weighed to ensure a 10 that a loading of 1 mg cm<sup>-2</sup> was achieved. The dried electrode was then either used as prepared or placed between baking paper and pressed at 40 bar (0.45 kN cm<sup>-2</sup>), 130 °C for 90 s using a Polystat 300S laboratory-scale press. In the case of sintering, the electrode was placed within a muffle furnace and sintered for 15 min at 340 °C. The sintering temperature of 340 °C was chosen as it is just below the melting point of PTFE. In such a way, the PTFE only 'softens' and induces improved bonding. Higher temperatures could lead to a full closure of the pores by liquid PTFE or decomposition of the binder. The lower pressing temperature as compared to the PTFE melting point was likewise selected for the pressing process, because the press cannot technically be operated at 340 °C and no decomposition of components such as methyl cellulose should take place during pressing.

From the different electrodes, 22 mm circular electrodes were cut out and each of those was drop coated with 133  $\mu$ l Sustainion XA-9 and dried overnight under atmospheric conditions. Before electrocatalysis



experiments, the electrodes were put into 1 M KOH for activation for 24 h by converting the  $Cl^{-}$  form of Sustainion XA-9 into the  $OH^{-}$  form.



## Electrochemical characterization and product analysis

The electrochemical characterization was performed using an inhouse-built three compartment cell with a cathode and anode chamber being separated by a Fumasep F-10120-PK membrane. The prepared GDEs were used as cathodes with catalyst facing the electrolyte solution. A nickel wire was utilized as counter electrode and a reversible hydrogen electrode (HydroFlex®) was used as a reference electrode for electroless potential determination. For all experiments, 1 M KOH was used as electrolyte. Electrolysis was then performed by chronopotentiometry. The geometric active area was 2.011 cm<sup>2</sup> and 200 mA cm<sup>-2</sup> were applied. The GDE was then fed with CO<sub>2</sub> and Ar as internal standard on the gas side. The CO<sub>2</sub> flow rate was

22.5 ml min<sup>-1</sup> (for Ar 2.5 ml min<sup>-1</sup>), and the backpressure was set to be 25 mbar during the electrolysis experiment. Between the cell and the GC, the gas stream was purged through a water-filled, ice-cooled trap to accumulate condensable products and to detect product crossover through the GDE. All measurements were carried out using a Gamry Interface 1010 potentiostat and a GC-MS QP2020 (Shimadzu; carrier gas helium; column: Carboxen 1010 PLOT from Supelco).

Acid products were analyzed using an Agilent Technologies HPLC 1200 with diode array detector (DAD detector 210 nm  $R_{eff}$  360 nm) and a Phenomenex Rezex ROA-Organic Acid H+ (8%) 250 × 4.6 nm column. The injection volume was 20  $\mu$ l, the column temperature was 60 °C, and 5 mM H<sub>2</sub>SO<sub>4</sub> was used as eluent with a flow rate of 0.2 ml min<sup>-1</sup>. The electrolyte samples were diluted with 5 mM H<sub>2</sub>SO<sub>4</sub>. An Agilent 7890B gas chromatograph with MSD 5977B and Agilent 7697A headspace sampler was used for alcohol analysis and 2.5 ml of the sample was placed in a headspace vial, mixed with an internal standard

alcohol analysis and 2.5 ml of the sample was placed in a headspace vial, mixed with an internal s solution. A DB 624 UI 30 m  $\times$  0.32 mm  $\times$  1.8  $\mu$ m was used as the column.

### Physical characterization

Rheological investigations were carried out using a Modular Compact Rheometer-102 (Anton Paar). A cone/plate attachment has been used.

SEM-EDX measurements were carried out using a ZEISS Gemini2 Merlin. SEM images were recorded at 5 kV, for SEM-EDX 20 kV were used. The electrodes were coated with carbon before.

X-ray diffraction was performed using a PANalytical X-Pert MPD with Cu-K $\alpha$  radiation at 45 kV and 40 mA without using a monochromator. A step size of 0.79 s per step was chosen.

For the determination of metal loading by ICP-OES, the catalyst was first dried at 105 °C in a drying oven, then 100 mg of the sample was digested with 10 ml of HNO<sub>3</sub> Suprapur in a microwave at 230 °C for 30 min. ICP-OES measurements were performed using an 'Arcos' device with radial plasma. For every measurement as an internal standard, 20 mg  $1^{-1}$  yttrium was added to each sample and each calibration solution serving as a blank.

The evaluations were carried out using the Cu emission lines  $\lambda = 324.754$  nm and  $\lambda = 327.396$  nm and the Zn emission lines  $\lambda = 213.856$  nm and  $\lambda = 206.200$  nm. For calibration, 11 different Cu and Zn containing standards were used, with concentrations ranging between 0 and 40 mg l<sup>-1</sup>.

### Data availability statement

The data generated and/or analyzed during the current study are not publicly available for legal/ethical



reasons but are available from the corresponding author on reasonable request.



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